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**Description****Field of the Invention**

5 The invention relates to laminates for use as housewrap in the construction industry for house and office building to improve insulation and provide a water barrier.

**Related Art**

10 One commercially available housewrap film is a single layer of high density polyethylene flash spun into fibers and pressed to form the film. Another commercially available film employed as a housewrap is melt blown, spun-bonded polyethylene.

Yet another housewrap material is made of polyethylene film attached to a supporting mesh to provide improved strength. The material has tiny holes punctured in it so as to avoid water ingress but permit breathing.

15 All of the aforementioned materials fail in certain severe tests when water stands in a hollow formed by the film and surfactant is present. Water drips through rapidly.

The invention has amongst its aims that of providing a material which is strong, has a good balance breathability and barrier characteristic and which will resist ingress of water even in extreme circumstances.

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**Summary of Invention**

In a first aspect, the invention provides a composite breathable laminate suitable for use as a housewrap comprising a breathable polyolefin film laminated to a non-woven fabric, characterised in that

25 a. the film comprises from 15 to 35% by volume of a pore nucleating filler based on the polyolefin/filler combination,  
b. the film comprises interconnected voids at the filler sites.

In a second aspect, the invention provides a method of preparing a composite breathable laminate suitable for use as a housewrap comprising:  
30 extruding a breathable film of polyolefin containing from 15 to 35% by volume of a pore nucleating filler based on the polyolefin/filler combination,  
stretching said film to cause said filler to be pulled away from said polyolefin to form interconnected voids, and  
laminating said film with a breathable non-woven fabric.

35 The porous polyolefin layer may be produced by known procedures. A precursor film filled with calcium carbonate can be stretched to give "Breathable" films which are gas/vapour permeable and liquid impermeable and is described in US Patent No. 4,472,328 assigned to Mitsubishi Chemical Industries Ltd. The Mitsubishi patent describes a breathable polyolefin film prepared from a polyolefin/filler composition having from 20 percent to 80 percent by weight of a filler such as a surface treated calcium carbonate. A  
40 liquid of waxy hydrocarbon polymer elastomer such as a hydroxy-terminated liquid polybutadiene was found to produce a precursor film that could be monoaxially or biaxially stretched to make a film breathable. The breathable film described by Mitsubishi is also described in Great Britain Patent No. 2,115,702 assigned to Kao Corporation. New films in which the film is embossed and stretched as described in this specification can also be used.

45 The open structure may be a commercially available material. Nonwoven cross-laminated fibrillated film fabrics of high density polyethylene are also known such as, for example, as described in U.S. Patent 4,681,781 assigned to C-I-L Inc., and are commercially available, for example, under the trade designation CLAF® from Conwed Plastics. The CLAF films, for example, are spread during the manufacturing process therefor and then laminated at the crossing points to form a thin, open mesh fabric of good strength and durability.

50 In the invention porous polyolefin films, used largely for diaper like applications, are combined with backing structure by lamination in a manner largely preserving the film porosity to provide a combined sheet-like material which has very useful properties in housewrap applications.

Composite laminates of the invention have good breathability and improved strength and other properties. Such a laminate can be formulated to provide high water vapour permeability and yet has a low permeability to air and high break strength, tear strength and puncture strength.

Breathable housewrap laminates can be made which have a water vapour transmission rate as determined in accordance with ASTM F372-73, of at least 1000 g/m<sup>2</sup> per day, such as 3000 g/m<sup>2</sup> per day.

and preferably at least 6000 g/m<sup>2</sup> per day, and especially at least 8000 g/cm<sup>2</sup> per day, and a Gurley resistance to air permeability not less than 100 s/100ml. The laminate resists the passage of water even in the presence of surfactant like materials.

The breathable film used in the laminate of the present invention is produced from a precursor film that is prepared from a polymer composition that comprises at least a polyolefin component and a filler. The polyolefin component may be any polyolefin which is suitable for film production, such as polypropylene, copolymers of propylene, homopolymers and copolymers of ethylene or blends thereof. A preferred polyolefin is a copolymer of ethylene and other alpha-olefins having from 3 to 18 carbons atoms, and particularly preferred is linear low density polyethylene.

Linear low density polyethylene (LLDPE) is produced by copolymerizing ethylene with C<sub>4</sub> to C<sub>10</sub> alpha-olefin.

Generally the preferred alpha-olefins include those selected from the group comprising butene-1, pentene-1, hexene-1, 4-methylpentene-1, heptene-1, and octene. The comonomers may be present in amounts up to 20 wt. %, normally between 3 and 14 wt%.

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#### DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS OF THE INVENTION

The invention is a laminate of a breathable polyolefin film and a fabric. Suitable breathable polyolefin films used in the laminate of the present invention should preferably have a water vapor transmission rate as determined in accordance with ASTM F372-73, of at least 1000 g/m<sup>2</sup> per day, preferably at least about 20 3000 g/m<sup>2</sup> per day, and especially at least 6000 or 8000 g/m<sup>2</sup> per day, and a Gurley resistance to air permeability not less than 100 s/100ml, and preferably not less than about 500 s/100ml.

Polymerization to form LLDPE may be conducted at low pressure using a chromium catalyst or Ziegler catalyst and may be carried out in the gas phase. The LLDPE produced by such methods have a density between 0.900 and 0.935 g/cm<sup>3</sup> and a melt index (MI) between 0.1 and 5.0 grams per 10 minutes. Manufacturing processes for production of LLDPE are known, such as disclosed in U.S. Patent Nos. 4,076,698 and 4,205,021. LLDPE is preferred as the polyolefin film component for use in the laminate of this invention because of its high tear strength, ease of compounding, and low cost. However, it is contemplated that ultra low density polyethylene or plastomers are also suitable for use as the film component.

Fillers useful in the breathable film of the laminate of this invention may be any inorganic or organic material having a low affinity for and a significantly lower elasticity than the polyolefin component. Preferably the filler should be a rigid material having a non-smooth hydrophobic surface, or a material which is treated to render its surface hydrophobic. The preferred mean average particle size of the filler is between about 3 to 5 µm for films having a thickness of between 102-152 µm (4-6 mil) prior to stretching.

Examples of the inorganic fillers include calcium carbonate, talc, clay, kaolin, silica, diatomaceous earth, magnesium carbonate, barium carbonate, magnesium sulfate, barium sulfate, calcium sulfate, aluminum hydroxide, zinc oxide, magnesium hydroxide, calcium oxide, magnesium oxide, titanium oxide, alumina, mica, glass powder, zeolite, silica, clay, etc. Calcium carbonate is particularly preferred for low cost, whiteness, inertness, and availability. The inorganic fillers such as calcium carbonate are preferably surface treated to be hydrophobic so that the filler can repel water to reduce agglomeration of the filler. Also, the surface coating should facilitate dispersion of the filler in the polymer while allowing the filler to be pulled away from the polyolefin under stress. A preferred coating agent is calcium stearate which is FDA approved and readily available. Organic fillers such as wood powder, pulp powder, and other cellulose type powders may be used. Polymer powders such as Teflon® powder and Kevlar® powder can also be used.

The amount of filler added to the polyolefin depends on the desired properties of the breathable film including tear strength, water vapor transmission rate, and stretchability. However, it is believed that a breathable film cannot be produced as is taught herein with an amount of filler less than about 15 percent by volume of the polyolefin/filler composition (e.g. LLDPE/CaCO<sub>3</sub> having less than about 38 percent by weight CaCO<sub>3</sub>). The minimum amount of filler is needed to insure the interconnection within the film of voids created at the situs of the filler, particularly by the stretching operation to be subsequently performed on the precursor film. Further, it is believed that useful films could not be made with an amount of the filler in excess of about 35 percent by volume of the polyolefin/filler composition (e.g. LLDPE/CaCO<sub>3</sub> having greater than about 65 percent by weight CaCO<sub>3</sub>). Higher amounts of filler may cause difficulty in compounding and significant losses in strength of the final breathable film.

Polyolefin/filler compositions usable in the breathable film of the laminate of this invention may be compounded in several different ways. The components may be brought into intimate contact by, for example, dry blending these materials and then passing the overall composition through a compounding extruder. Alternatively, the polyolefin and filler components may be fed directly to a mixing device such as

a compounding extruder, high shear continuous mixer, two roll mill or an internal mixer such as a Banbury® mixer. Overall, the objective is to obtain a uniform dispersion of the filler in the polymer without agglomeration, and this is readily achieved by inducing sufficient shear and heat to cause the polyolefin component to melt. However, time and temperature of mixing should be controlled as is normally done to 5 avoid molecular weight degradation. Compounding of LLDPE and calcium carbonate that is surface treated with calcium stearate has been improved by vacuum drying the mixture within the extruder.

The tear strength and softness of a film prepared from the polyolefin/filler composition may be improved by addition of small amounts of an olefinic elastomer.

The film forming composition may be manufactured into a precursor film by conventional tubular extrusion (blown bubble process), by cast extrusion or by quenching techniques which are well known in the art. Film formation by cast extrusion is preferred because the cast film can be immediately melt embossed as described below.

In the cast extrusion process, the molten resin is extruded from an elongate die in the form of a web. The web is pressed against a cold roll to chill and solidify the film. An embossed pattern may be imparted 15 on the film utilizing an engraved roll. The precursor film is preferably produced to a gauge of 102-152 µm (4 to 6 mils), which allows for further stretching as described below. The extrusion temperatures, die temperatures, and embossing roll temperatures will depend on the composition employed, but generally will be in the following ranges for compositions of the present invention prepared by cast extrusion:

20	Melt Temperature	177-232 °C (350-450 °F)
	Die Temperature	177-232 °C (350-450 °F)
	Embossing Roll Temperature	21-54 °C (70-130 °F)

25      Film formation by tubular extrusion produces balanced films having increased film strength in both the machine and cross-machine direction. In the tubular blown film process, the film forming composition is first melted and then extruded through an annular die. The die should preferably have a die gap suitable for extruding LLDPE resin which normally is greater than about 0.5 mm and preferably greater than 0.75 mm. The film forming composition is extruded at a melt temperature between about 150 °C to 300 °C, preferably 30 between 190 °C and 240 °C. The molten composition is preferably extruded in an upward vertical direction in the form of either a bubble or a tube, although it also can be extruded either downwardly or horizontally. The tubular extrudate is expanded to the desired dimensions and then cooled by one of several conventional techniques which are well known in the art, e.g., forced air, mandrel, and water quench. The tubular film, or bubble, is then flattened by passing the film through a collapsing frame and a set of nip rolls. 35      The nip rolls are driven, thereby proving a means of drawing the tubular film or bubble away from the annular die.

A positive pressure of a gas, such as air or nitrogen, is maintained inside the tubular bubble. As is known in the operation of conventional blown film processes, the presence of the gas is controlled to impart a desired dimensional orientation to the film tube or bubble. The degree of tubular bubble expansion may 40 be measured as the ratio of the expanded bubble circumference to the circumference of the die annulus. This ratio is generally in the range of 1:1 to 6:1 and for a precursor breathable film is preferably from 2:1 to 4:1.

45      Embossing is typically used on the surface of polyolefin films to reduce gloss. Embossing can be imposed on the precursor film surface at the time of the film fabrication for cast extrusion, or at a subsequent time for cast or tubular extrusion by procedures well known in the art. For the present breathable film used in the laminate of the invention, embossing imposes a pattern of different film thicknesses within the precursor film, and can be conducted with any micro/macro pattern, e.g. cross-hatching, dots, lines, circles, diamonds, hexagons etc. The pattern can be either in line and/or off line and the rolls can be engraved with either pin up and/or pin down type configurations.

50      Final preparation of a breathable film for use in the present laminate is achieved by stretching the precursor film to form interconnected voids. Stretching or "Orientation" of the film may be carried out monoaxially in the machine direction (MD) or the transverse direction (TD) or in both directions (biaxially) either simultaneously or sequentially using conventional equipment and processes following cooling of the precursor film.

55      Blown films are preferably stretched in the machine direction or in both directions whereas cast films are preferably stretched in the transverse direction. For orientation in the MD, the precursor film is passed around two rollers driven at different surface speeds and finally to a take up roller. The second driven roller which is closest to the take up roll is driven faster than the first driven roller. As a consequence the film is

stretched between the driven rollers.

Film orientation may also be carried out in a tentering device with or without MD orientation to impart TD orientation to the film. The film is gripped by the edges for processing through the tentering device. Stretching of melt embossed precursor films with a tentering device at a film speed of about 60 meters per minute produced breathable films having the desired water vapor and permeabilities. The resulting films had greater permeability in the areas of reduced thickness in comparison to the areas of greater thickness.

Although not thoroughly investigated, controlling of the strain on the film during stretching is believed to be important to controlling the permeability. For stretching in the transverse direction, strain can be controlled for a given stretch ratio by adjusting the film speed and the stretching distance. The stretching distance is measured, between the point where the film starts to increase in width to the closest point where the film is fully stretched. For stretching in the machine direction, strain can be controlled for a given stretch ratio by controlling film speed and the gap between the first and second driven rollers.

A range of stretching ratios from 1:2 to 1:5 prove satisfactory for MD stretching with a ratio of 1:4 being preferred. A range of stretching ratios of 1:2 to 1:5 prove satisfactory for TD stretching with a ratio of 1:4 being preferred.

The water vapor permeability of the embossed film following stretching, as measured by the final WVTR of the film, was found to be inversely related to the stretching temperature. Stretching at a temperature of about 45°C produced a film having a slightly higher WVTR than stretching at temperatures of about 60°C.

The stretched film can be heat set to stabilize the film for any subsequent processing at temperatures above the stretching temperature. The film can be heat set at any temperature above the stretching temperature and below the softening temperature to add stability. However, higher temperatures cause stiffness and some reduction in WVTR. Heat setting at about 80°C produced a softer film with substantially higher WVTR in comparison to heat setting at about 95°C.

It is preferred that tension be maintained on the film during the heat setting and cooling to minimize shrinkback. Upon cooling to ambient temperature (i.e., room temperature) or near ambient, the holding force may be released. The film may contract somewhat (snapback) in the TD but will retain a substantial portion of its stretched dimension.

Heat setting can be accomplished by maintaining the film under tension in the stretched condition at the heat setting temperature for about 1 - 2 minutes. Preferably, however, the heat setting and cooling is carried out while permitting the film to contract slightly, but still under stress. The controlled shrinkback of from 5 to 30%, preferably between 15 and 25%, of the maximum stretched width has given particularly good results in eliminating storage shrinkage.

Fabrics suitably laminated to the breathable film in the housewrap of the present invention include any high strength fabric which can be bonded to the breathable film without adversely affecting the water vapor permeability or the resistance to air permeability of the breathable film, i.e. the fabric must generally have a suitably open mesh to avoid substantially blocking the micropores of the breathable film. The fabric is nonwoven polyolefin such as, for example, low density polyethylene, polypropylene, and preferably linear, low density polyethylene or high density polyethylene. The preferred fabric has an elongation (ASTM D1682) less than about 30%; an Elmendorf tear strength (ASTM D689) of at least 300 g, preferably at least 600g and especially at least 900g; and a breakload (ASTM D1682) of at least 268 kg/m (15 lb/in.), preferably at least 447 kg/m (25 lb/in.), and especially at least 536 kg/m (30 lb/in.). Suitable fabrics can be prepared from HDPE films having outer heat seal layers e.g. of ethylene-vinyl acetate coextruded on either side of the HDPE. The films are fibrillated, and the resulting fibers are spread in at least two transverse directions at a strand count of 2-4 per cm (6-10 per inch). The spread fibers are then cross-laminated by heat to produce a nonwoven fabric of 76-127 µm (3-5 mils) with about equal MD and TD strength. These fabrics have excellent strength properties in both MD and TD for reinforcing the breathable film, an open structure to avoid substantially blocking the micropores of the breathable film when laminated thereto, and an outer heat seal layer of e.g. ethylene-vinyl acetate copolymer.

The fabric and the breathable film are laminated together to form the breathable composite of the invention. The lamination may be effected by facing the film and the fabric together and applying heat and pressure. The laminating temperatures to which the film and fabric are exposed should be sufficient to achieve lamination, but should not be too high in order to avoid the flow of the film polymer into the microporous spaces and a consequent reduction in water vapor transmissibility. In a preferred embodiment, the fabric is heated on a hot roller, preferably at 93-116°C (200-240°F), and then pressed, preferably at a pressure of about 35-70 N/cm² (50-100 psi), into contact with the unheated film to bond the fabric and film into the laminate.

Preferred fabrics are commercially available under the trade designations CC-1001, CC-2001 and CC-3001 CLAF® nonwoven HDPE fabrics.

EXAMPLES

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The following examples, which illustrate melt embossed breathable films and fabric laminates thereof prepared in accordance with the present invention, are not intended to limit the invention to the specific compositions. Other compounds such as elastomers, stabilizers against heat or ultraviolet rays, pigments, antistatic agents, etc. may be added to the compositions in the conventional manner. In the examples which follow water vapor transmission rates (WVTR) were measured in accordance with ASTM F372-73 using a Permatran® W1 analyzer manufactured by Modern Controls International, Inc. and air resistance was measured on a Gurley® H-P-S Tester No. 4200 in accordance with the manufacturer's directions.

Example 1 (COMPARISON)

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A linear low density polyethylene which consisted of a copolymer of ethylene and hexene-1 was compounded with an equal weight of a surface treated calcium carbonate. The calcium carbonate was surface treated with calcium stearate to render the surface of the particles hydrophobic. The resulting formulation was cast extruded into a precursor film having a thickness of approximately 102-152 µm (4 to 6 mil).

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The resulting precursor film was cooled and then subjected to tentering stress in the transverse direction with a stretch ratio of 4 to 1 and a film speed of about 60 meters per minute. Stretching was performed in a tentering frame with heat applied only to the final zone of the tentering frame. The temperature of the film in the final zone was maintained at about 93 °C. As a result of convection within the 25 tentering frame, stretching of the film occurred at approximately 60 °C. The film became white and breathable when stretched and retained those properties following the heat setting treatment. The final breathable film had a water vapor transmission rate of up to 5800 grams per square meter per day at 38 °C.

Example 2

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The LLDPE/calcium carbonate composition of Example 1 was cast extruded under the same conditions as Example 1. The precursor film was passed between a smooth roller and a diamond patterned embossing roller. The resulting film had a thickness of approximately 102-152 µm (4 to 6 mil) and a diamond pattern on one side. The film became whiter when stretched at the temperature and conditions stated for Example 35 1. Heat setting was also conducted as described for Example 1. This film had a WVTR value of 8,100 grams per square meter per day. Stretching caused greater permeability in the thin portions of the film created by the embossing roll in comparison to the thick area which retained greater strength. The final film had a drapy and softer film structure and a higher tear strength than the film of Example 1.

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Example 3

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The LLDPE/filler composition of Example 1 was extruded and melt embossed under the same conditions of Example 2. The precursor film was then stretched with the tentering device of Example 2. The temperature of the film in the heat setting zone was maintained at about 78 °C and stretching occurred at about 35 °C. The final film had a WVTR value of 10,300 grams per square meter per day.

Example 4

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A breathable film was prepared under the same conditions of Example 3 except that the stretching temperature was adjusted to 70 °C. The final film had a WVTR value of 10,000 grams per square meter per day.

Example 5

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A breathable film was prepared under the same conditions of Example 3 except that the stretching temperature was adjusted to 93 °C. The final film had a WVTR value of 9,900 grams per square meter per day.

The following Table 1 presents a comparison of the variables in Examples 1-5.

TABLE 1

	Stretch Temp., °C	Heat Set Temp., °C	WVTR g/m <sup>2</sup> /day	
5	Example 1 (Comparison)	60	93	5,800
	Example 2	60	93	8,100
	Example 3	35	78	10,300
	Example 4	70	78	10,000
10	Example 5	93	78	9,900

Examples 6-19

15 Various breathable films ("BF") prepared in the manner described above under the conditions indicated in Table II (50wt% LDPE/50 wt. % CaCO<sub>3</sub>) were heat laminated with commercially available CLAF® nonwoven fabrics designated CLAF-1001, CLAF-2001, CLAF-3001 and CLAF-5001 having the properties indicated in Table II. The CLAF® fabrics had a heat seal layer comprising ethylene-vinyl acetate copolymer. The breathable films and fabrics were heat laminated by heating the fabric to 93-116 °C (200-240 °F) and pressing the unheated BF to the heated fabric between rollers at 70 N/cm<sup>2</sup> (100 psi). Two commercially 20 available housewraps, with the trade designations BARRICADE® (spun-bonded polyethylene) and TYVEK® (flash spun HDPE) are included in Table II as Examples 18 and 19 for purposes of comparison.

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TABLE II WTR<sub>2</sub> & GURLEY AIR RESISTANCE TESTS

Example	Film/ Fabric/ Composite	Stretch Temp. °C / °F	Heat Set Temp. °C / °F	Laminating Temp. °C / °F	Weight g/m <sup>2</sup>	Water vapor transmissibility @ 37.8°C (g/m <sup>2</sup> /day)	Gurley Air Resistance (sec./100 ml)	Breakload (lb/in.) HD / TD	Elongation (Y) HD / TD	Elongation (S) HD / TD
6	BF	40 (115)	90 (205)	--	13.4 (0.4)	8000	500	46.0 (2.5)	1260 (45)	100 (10)
7	CLAF-1001	--	--	47.5 (1.4)	--	--	--	56.3 (32)	25 (30)	939 (963)
8	Ex. 6 + CLAF-1001	90 (175)	90 (205)	114 (240)	56.1 (2.6)	6000	66.9 (38)	151 (37)	27 (30)	1200 (1400)
9	BF	80 (175)	90 (205)	--	17.6 (0.5)	8000	500	44.0 (2.5)	1260 (45)	100 (10)
10	CLAF-3001	--	--	23.7 (0.7)	--	--	--	34.4 (15)	18 (21)	427 (51)
11	Ex. 9 + CLAF-3001	--	--	107 (225)	64.0 (1.9)	6400	600	15.2 (20)	475 (27)	16 (24)
12	BF	--	--	57.0 (0.5)	3600	3000	31.1 (12)	32.4 (1.3)	90 (20)	200 (180)
13	CLAF-2001	--	--	39.5 (0.9)	--	--	--	33.4 (19)	22 (29)	624 (605)
14	Ex. 12 + CLAF-2001	--	--	27.4 (2.0)	--	--	--	47.5 (27)	21 (23)	600 (660)
15	CLAF-5001	--	--	13.6 (0.4)	--	--	--	46.5 (10.5)	19 (19)	139 (158)
16	Ex. 9 + CLAF-5001	--	--	47.5 (1.4)	--	--	--	47.5 (10.5)	19 (19)	139 (158)
17	Ex. 9 + CLAF-3001	--	104 (200)	107 (225)	67.8 (2.0)	6400	550	71.7 (18)	26.4 (15)	19 (15)
18	Barricade® Tyvek®	--	--	51.0 (1.5)	6500	800	4.91 (2.6)	52.8 (30)	24 (28)	1200 (1175)
19	--	--	--	67.6 (2.0)	9200	20	15.8 (9.0)	51.8 (30)	22 (26)	230 (260)
					10000	20	34.7 (22)	54.6 (31)	15 (20)	480 (460)

From the data seen in the foregoing Table II, it is readily apparent that the housewrap of the present invention is far superior to the commercially available housewrap, in both air resistance and tear strength, and comparable in water vapor transmissibility. Quite surprisingly, the breathable film/CLAF fabric laminates substantially retain the desirable water vapor transmissibility and air resistance of the breathable film, but yet generally have average tear, elongation and breakload properties better than either the breathable film

or the CLAF fabric, a truly synergistic result.

While the invention has been described as a housewrap, the laminated fabric and film is equally well suited for other applications, including for example, the manufacture of disposable absorbant fabrics such as diapers and devices for incontinents medical and surgical supplies, apparel and household furnishings, tape and packaging, and filtration membranes. Specific examples may include burn dressings, sterile packaging, rain coats, shoe linings, nonfogging packaging film, bacteria filters, water purification filters and the like.

### Claims

10. 1. A composite breathable laminate suitable for use as a housewrap comprising a breathable polyolefin film laminated to a non-woven fabric, characterised in that
  - a. the film comprises from 15 to 35% by volume of a pore nucleating filler based on the polyolefin/filler combination,
  - b. the film comprises interconnected voids at the filler sites.
15. 2. A laminate according to claim 1 wherein said fabric is of polyolefin selected from high density polyethylene, polypropylene and linear low density polyethylene.
20. 3. A laminate according to claim 1 or claim 2 wherein the fabric layer of the laminate has an outer heat seal layer.
25. 4. A laminate according to any preceding claim wherein said fabric is of high density polyethylene film fibrillated and with the resulting fibers spread in at least two transverse directions and cross-laminated, and having outer heat seal layers on each side, the fabric having MD and TD strand counts of from 2 to 4 per cm (6 to 10 per inch) and a thickness from 76 to 127 µm (3 to 5 mils).
30. 5. A laminate according to claim 3 or claim 4 wherein said heat seal layer or layers is of ethylene vinyl acetate copolymer.
35. 6. A laminate according to any preceding claim wherein said fabric has an elongation less than 30%, an Elmendorf tear strength of at least 300 g, and a break load of at least 268 kg/m (15 lb/inch.)
40. 7. A laminate according to any preceding claim wherein said film has a water vapour transmission rate of at least 1000 g/m<sup>2</sup> and a Gurley air resistance rate not less than 100 s/100ml.
45. 8. A laminate according to any preceding claim wherein said film has a water vapour transmission rate of at least 8000 g/m<sup>2</sup> and a Gurley air resistance rate not less than 500 s/100ml.
50. 9. A laminate according to any preceding claim wherein said film is of a copolymer of polyethylene and a C<sub>4</sub>-<sub>10</sub> alpha-olefin.
55. 10. A laminate according to any preceding claim wherein said film is of linear low density polyethylene.
11. A laminate according to any preceding claim wherein said filler is of calcium carbonate surface treated with a hydrophobic coating agent.
12. A laminate according to any preceding claim wherein said film is embossed.
13. A method of preparing a composite breathable laminate suitable for use as a housewrap comprising:
  - extruding a breathable film of polyolefin containing from 15 to 35% by volume of a pore nucleating filler based on the polyolefin/filler combination,
  - stretching said film to cause said filler to be pulled away from said polyolefin to form interconnected voids, and
  - laminating said film with a breathable non-woven fabric.
14. A method according to claim 13 wherein said fabric is as defined in any one of claim 2 to 6.

15. A method according to claim 13 or claim 14 wherein said film is as defined in any one of claims 7 to 12.
16. A method according to any of claims 13 to 15 wherein said filler is of calcium carbonate surface treated  
5 with a hydrophobic coating agent.

**Patentansprüche**

1. Atmungsfähiges Verbundlaminat, das zur Verwendung als Hausumhüllung geeignet ist und eine  
10 atmungsfähige Polyolefinfolie umfaßt, die auf einen Vliesstoff laminiert ist, dadurch gekennzeichnet, daß  
a. die Folie 15 bis 35 Vol.-% eines porenbildenden Füllstoffs, bezogen auf die Polyolefin/Füllstoff-  
Kombination, und  
b. die Folie miteinander verbundene Hohlräume an den Füllstoffstellen umfaßt.
15. 2. Laminat nach Anspruch 1, bei dem der Stoff aus Polyolefin ausgewählt aus Polyethylen hoher Dichte,  
Polypropylen und linearem Polyethylen niederer Dichte besteht.
3. Laminat nach Anspruch 1 oder Anspruch 2, bei dem die Stoffschicht des Laminats eine äußere  
Heißsiegelschicht aufweist.  
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4. Laminat nach einem der vorhergehenden Ansprüche, bei dem der Stoff aus fibrillierter Polyethylenfolie  
hoher Dichte besteht, wobei die resultierenden Fasern in mindestens zwei Querrichtungen ausgebreitet  
und über Kreuz laminiert sind und auf jeder Seite der Folie äußere Heißsiegelschichten vorhanden sind,  
wobei der Stoff MD- und TD-Strangzahlen von 2 bis 4 pro cm (6 bis 10 pro inch) und eine Dicke von  
25 76 bis 127 µm (3 bis 5 mils) aufweist.
5. Laminat nach Anspruch 3 oder Anspruch 4, bei dem die Heißsiegelschicht oder -schichten aus Ethylen-  
Vinylacetat-Copolymer bestehen.
30. 6. Laminat nach einem der vorhergehenden Ansprüche, bei dem der Stoff eine Dehnung von weniger als  
30 %, eine Elmendorf-Reißfestigkeit von mindestens 300 g und eine Bruchbelastung von mindestens  
268 kg/m (15 lb/inch) aufweist.
7. Laminat nach einem der vorhergehenden Ansprüche, bei dem die Folie eine Wasserdampfdurchgangs-  
35 rate von mindestens 1000 g/m<sup>2</sup> und eine Gurley-Luftwiderstandsrate von nicht weniger als 100 s/100 ml  
aufweist.
8. Laminat nach einem der vorhergehenden Ansprüche, bei dem die Folie eine Wasserdampfdurchgangs-  
40 rate von mindestens 8 000 g/m<sup>2</sup> und eine Gurley-Luftwiderstandsrate von nicht weniger als 500 s/100  
ml aufweist.
9. Laminat nach einem der vorhergehenden Ansprüche, bei dem die Folie aus einem Copolymer aus  
Polyethylen und einem C<sub>4-10</sub>- $\alpha$ -Olefin besteht.
45. 10. Laminat nach einem der vorhergehenden Ansprüche, bei dem die Folie aus linearem Polyethylen  
niederer Dichte besteht.
11. Laminat nach einem der vorhergehenden Ansprüche, bei dem der Füllstoff aus Calciumcarbonat  
50 besteht, das mit einem hydrophoben Beschichtungsmittel oberflächenbehandelt ist.
12. Laminat nach einem der vorhergehenden Ansprüche, bei dem die Folie geprägt ist.
13. Verfahren zur Herstellung eines atmungsfähigen Verbundlaminats, das zur Verwendung als Hausumhül-  
lung geeignet ist, bei dem:  
55 eine atmungsfähige Folie aus Polyolefin extrudiert wird, die 15 bis 35 Vol.-% an porenbildendem  
Füllstoff enthält, bezogen auf die Polyolefin/Füllstoff-Kombination,  
die Folie gestreckt wird, damit der Füllstoff von dem Polyolefin weggezogen wird, um miteinander  
verbundene Hohlräume zu bilden, und

die Folie mit einem atmungsfähigen Vliesstoff laminiert wird.

14. Verfahren nach Anspruch 13, bei dem der Stoff wie in einem der Ansprüche 2 bis 6 definiert ist.
- 5 15. Verfahren nach Anspruch 13 oder Anspruch 14, bei dem die Folie wie in einem der Ansprüche 7 bis 12 definiert ist.
- 10 16. Verfahren nach einem der Ansprüche 13 bis 15, bei dem der Füllstoff aus Calciumcarbonat besteht, das mit einem hydrophoben Beschichtungsmittel oberflächenbehandelt ist.

**Revendications**

1. Stratifié composite perméable aux gaz convenant pour l'utilisation comme revêtement pour le bâtiment, comprenant un film de polyoléfine perméable aux gaz stratifié à une étoffe non tissée, caractérisé en ce que
  - a. le film comprend 15 à 35 % en volume d'une charge de nucléation de pores, sur la base de l'association polyoléfine/charge,
  - b. le film comprend des vides interconnectés au niveau des sites de la charge.
- 20 2. Stratifié suivant la revendication 1, dans lequel l'étoffe est constituée d'une polyoléfine choisie entre un polyéthylène haute densité, un polypropylène et un polyéthylène linéaire basse densité.
3. Stratifié suivant la revendication 1 ou la revendication 2, dans lequel la couche d'étoffe du stratifié possède une couche thermosoudée extérieure.
- 25 4. Stratifié suivant l'une quelconque des revendications précédentes, dans lequel l'étoffe est constituée d'un film de polyéthylène haute densité fibrillé, avec les fibres résultantes étendues dans au moins deux directions transversales et soumises à une stratification croisée, et possédant des couches thermosoudées extérieures sur chaque face, l'étoffe ayant des nombres de filaments dans la direction machine et la direction transversale de 2 à 4 par cm (6 à 10 par inch) et une épaisseur de 76 à 127 µm (3 à 5 mils).
5. Stratifié suivant la revendication 3 ou la revendication 4, dans lequel la ou les couches thermosoudées sont constituées d'un copolymère éthylène-acétate de vinyle.
- 35 6. Stratifié suivant l'une quelconque des revendications précédentes, dans lequel l'étoffe possède un allongement inférieur à 30 %, une résistance au déchirement Elmendorf d'au moins 300 g et une charge de rupture d'au moins 268 kg/m (15 lb/in).
- 40 7. Stratifié suivant l'une quelconque des revendications précédentes, dans lequel le film possède un degré de transmission de vapeur d'eau d'au moins 1000 g/m<sup>2</sup> et un degré de résistance à l'air Gurley non inférieur à 100 s/100 ml.
8. Stratifié suivant l'une quelconque des revendications précédentes, dans lequel le film possède un degré de transmission de vapeur d'eau d'au moins 8000 g/m<sup>2</sup> et un degré de résistance à l'air Gurley non inférieure à 500 s/100 ml.
- 45 9. Stratifié suivant l'une quelconque des revendications précédentes, dans lequel le film est constitué d'un copolymère de polyéthylène et d'une alpha-oléfine en C<sub>4</sub> à C<sub>10</sub>.
- 50 10. Stratifié suivant l'une quelconque des revendications précédentes, dans lequel le film est constitué d'un polyéthylène linéaire basse densité.
11. Stratifié suivant l'une quelconque des revendications précédentes, dans lequel la charge est constituée d'un carbonate de calcium traité en surface avec un agent hydrophobe de revêtement.
- 55 12. Stratifié suivant l'une quelconque des revendications précédentes, dans lequel le film est gaufré.

13. Procédé de préparation d'un stratifié composite perméable à l'air convenant pour l'utilisation comme revêtement pour le bâtiment, comprenant :
  - l'extrusion d'un film de polyoléfine perméable à l'air, contenant 15 à 35 % en volume d'une charge de nucléation de pores, sur la base de l'association polyoléfine/charge,
  - 5 l'étirage dudit film pour provoquer l'expulsion de ladite charge hors de ladite polyoléfine pour former des vides interconnectés, et
  - la stratification dudit film à une étoffe non tissée perméable à l'air.
14. Procédé suivant la revendication 13, dans lequel l'étoffe répond à la définition suivant l'une quelconque des revendications 2 à 6.
15. Procédé suivant la revendication 13 ou la revendication 14, dans lequel le film répond à la définition suivant l'une quelconque des revendications 7 à 12.
16. Procédé suivant l'une quelconque des revendications 13 à 15, dans lequel la charge est constituée d'un carbonate de calcium traité en surface avec un agent hydrophobe de revêtement.

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